

REFERENCE: SF-340020

PROJECT: 17BP.5.R.69

STATE OF NORTH CAROLINA
DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	SF-340020	1	14

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STRUCTURE
SUBSURFACE INVESTIGATION

COUNTY FRANKLIN
PROJECT DESCRIPTION BRIDGE NO. 20 ON SR 1114
(PEACH ORCHARD RD.) OVER CEDAR CREEK

CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N. C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT (919) 707-6850. THE SUBSURFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

GENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORINGS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOISTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS MAY VARY CONSIDERABLY WITH TIME ACCORDING TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT. FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEPARTMENT DOES NOT WARRANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE, OR OPINION OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DEEMS NECESSARY TO SATISFY HIMSELF AS TO CONDITIONS TO BE ENCOUNTERED ON THE PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS ENCOUNTERED AT THE SITE DIFFERING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION.

- NOTES:
1. THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE N. C. DEPARTMENT OF TRANSPORTATION AS ACCURATE NOR IS IT CONSIDERED PART OF THE PLANS, SPECIFICATIONS OR CONTRACT FOR THE PROJECT.
 2. BY HAVING REQUESTED THIS INFORMATION, THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

PERSONNEL

TRIGON
GOODNIGHT, D.J.

INVESTIGATED BY DJG
DRAWN BY HILL, M.J.
CHECKED BY HUNSBERGER, W.S.
SUBMITTED BY FALCON ENG.
DATE OCTOBER 2017



SIGNATURE DATE

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT
SUBSURFACE INVESTIGATION
SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

SOIL DESCRIPTION										GRADATION										ROCK DESCRIPTION										TERMS AND DEFINITIONS																																																																																																																																																																										
<p>SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE, <i>VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6</i></p>										<p>WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE. UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.</p>										<p>HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED, AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:</p>										<p>ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER. AQUIFER - A WATER BEARING FORMATION OR STRATA. ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND. ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC. ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE. CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE. COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE. CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK. DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL. DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH. FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE. FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES. FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLOGGED FROM PARENT MATERIAL. FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM. FORMATION (FM) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD. JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED. LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT. LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS. MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE. PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM. RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK. ROCK QUALITY DESIGNATION (ROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE. SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK. SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS. SLICKENISE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE. STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (IN OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS. STRATA CORE RECOVERY (SREC.) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE. STRATA ROCK QUALITY DESIGNATION (SROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE. TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.</p>																																																																																																																																																																										
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CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.</p> <p>MODERATE (MOD.): SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.</p> <p>MODERATELY SEVERE (MOD. SEV.): ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK. <i>IF TESTED, WOULD YIELD SPT REFUSAL</i></p> <p>SEVERE (SEV.): ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES > 100 BPF</i></p> <p>VERY SEVERE (IV SEV.): ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES < 100 BPF</i></p> <p>COMPLETE: ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS ALSO AN EXAMPLE.</p>									
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<p style="text-align: center;">TEXTURE OR GRAIN SIZE</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th>U.S. STD. SIEVE SIZE OPENING (MM)</th> <td>4</td> <td>10</td> <td>40</td> <td>60</td> <td>200</td> <td>270</td> </tr> <tr> <td></td> <td>4.75</td> <td>2.00</td> <td>0.42</td> <td>0.25</td> <td>0.075</td> <td>0.053</td> </tr> <tr> <th>BOULDER (BLDR.)</th> <th>COBBLE (COB.)</th> <th>GRAVEL (GR.)</th> <th>COARSE SAND (CSE. SD.)</th> <th>FINE SAND (F SD.)</th> <th>SILT (SL.)</th> <th>CLAY (CL.)</th> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <th>GRAIN SIZE</th> <td>MM 305</td> <td>75</td> <td>2.0</td> <td>0.25</td> <td>0.05</td> <td>0.005</td> </tr> <tr> <td></td> <td>IN. 12</td> <td>3</td> <td></td> <td></td> <td></td> <td></td> </tr> </table>										U.S. STD. SIEVE SIZE OPENING (MM)	4	10	40	60	200	270		4.75	2.00	0.42	0.25	0.075	0.053	BOULDER (BLDR.)	COBBLE (COB.)	GRAVEL (GR.)	COARSE SAND (CSE. SD.)	FINE SAND (F SD.)	SILT (SL.)	CLAY (CL.)								GRAIN SIZE	MM 305	75	2.0	0.25	0.05	0.005		IN. 12	3					<p style="text-align: center;">ABBREVIATIONS</p> <p>AR - AUGER REFUSAL BT - BORING TERMINATED CL - CLAY CPT - CONE PENETRATION TEST CSE - COARSE DMT - DILATOMETER TEST DPT - DYNAMIC PENETRATION TEST e - VOID RATIO F - FINE FOSS. - FOSSILIFEROUS FRAC. - FRACTURED, FRACTURES FRAGS. - FRAGMENTS HI. - HIGHLY</p> <p>MED. - MEDIUM MICA - MICACEOUS MOD. - MODERATELY NP - NON PLASTIC ORG. - ORGANIC PMT - PRESSUREMETER TEST SAP. - SAPROLITIC SD. - SAND, SANDY SL. - SILT, SILTY SLI. - SLIGHTLY TCR - TRICONE REFUSAL w - MOISTURE CONTENT V - VERY</p> <p>VST - VANE SHEAR TEST WEA. - WEATHERED γ_u - UNIT WEIGHT γ_d - DRY UNIT WEIGHT</p> <p>SAMPLE ABBREVIATIONS</p> <p>S - BULK SS - SPLIT SPOON ST - SHELBY TUBE RS - ROCK RT - RECOMPACTED TRIAXIAL CBR - CALIFORNIA BEARING RATIO</p>																																																																																																																																																				
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<p style="text-align: center;">COLOR</p> <p>DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-BROWN). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.</p>										<p style="text-align: center;">INDURATION</p> <p>FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.</p> <p>FRIABLE: RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.</p> <p>MODERATELY INDURATED: GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER.</p> <p>INDURATED: GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER.</p> <p>EXTREMELY INDURATED: SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.</p>																																																																																																																																																																																														
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<p style="text-align: center;">FRAC. MARK: BL-3:</p> <p>N: 845037.5 E: 2182723.2</p> <p>STA. 13+37.37 OFFSET: 14.3' LT, -L- ELEVATION: 252.79 FEET</p>										<p style="text-align: center;">NOTES:</p> <p>FIAD - FILLED IMMEDIATELY AFTER DRILLING</p>																																																																																																																																																																																														

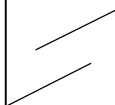
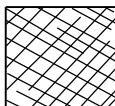


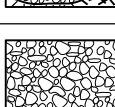
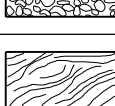
**NORTH CAROLINA DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT**

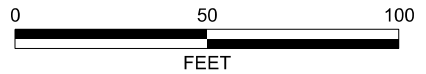
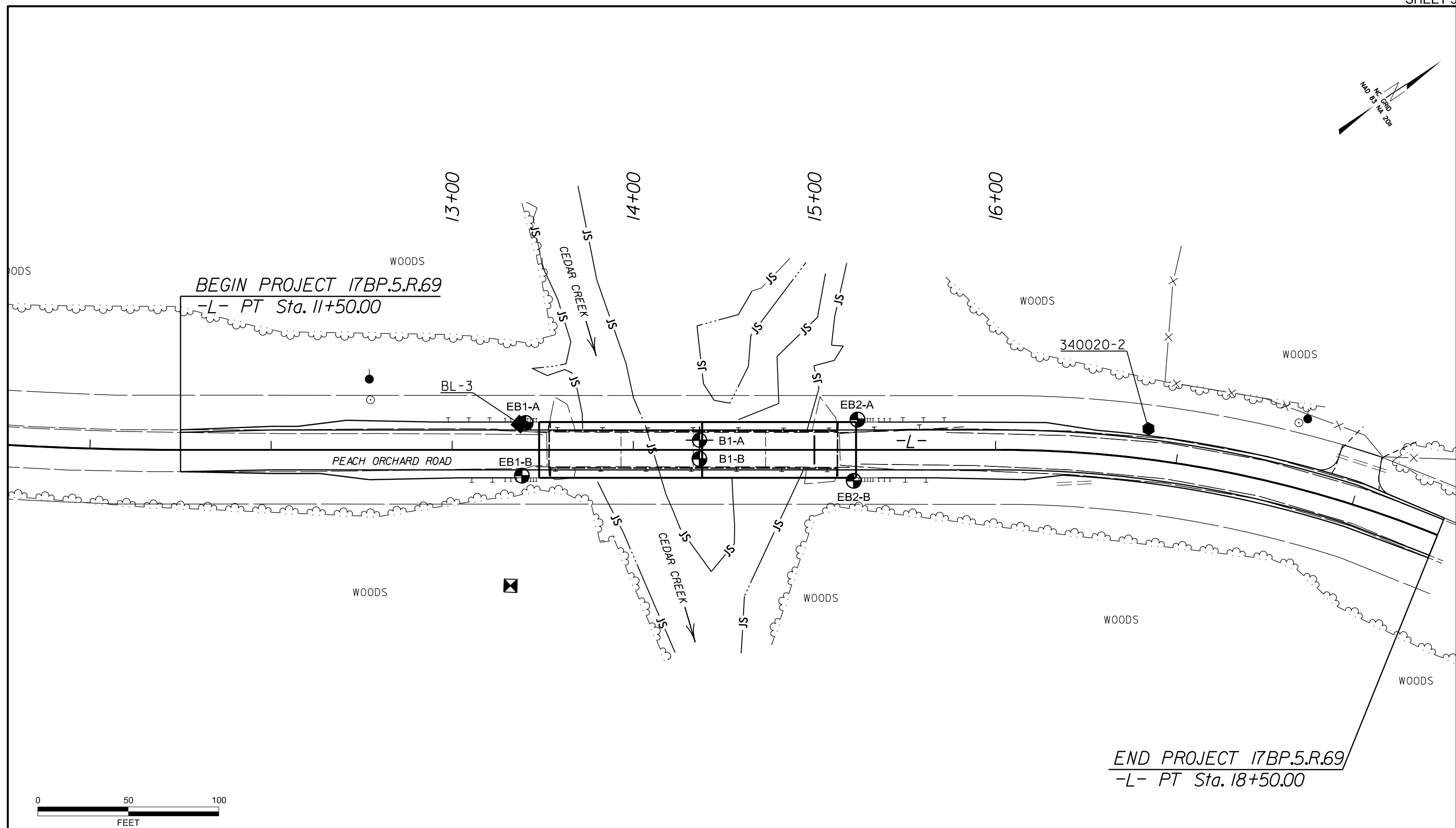
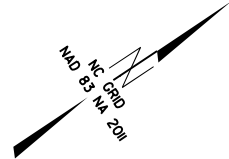
SUBSURFACE INVESTIGATION

**SUPPLEMENTAL LEGEND, GEOLOGICAL STRENGTH INDEX (GSI) TABLES
FROM AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS**

AASHTO LRFD Figure 10.4.6.4-1 — Determination of GSI for Jointed Rock Mass (Marinos and Hoek, 2000)

AASHTO LRFD Figure 10.4.6.4-2 — Determination of GSI for Tectonically Deformed Heterogeneous Rock Masses (Marinos and Hoek, 2000)

<p>GEOLOGICAL STRENGTH INDEX (GSI) FOR JOINTED ROCKS (Hoek and Marinos, 2000)</p> <p>From the lithology, structure and surface conditions of the discontinuities, estimate the average value of GSI. Do not try to be too precise. Quoting a range from 33 to 37 is more realistic than stating that GSI = 35. Note that the table does not apply to structurally controlled failures. Where weak planar structural planes are present in an unfavorable orientation with respect to the excavation face, these will dominate the rock mass behaviour. The shear strength of surfaces in rocks that are prone to deterioration as a result of changes in moisture content will be reduced if water is present. When working with rocks in the fair to very poor categories, a shift to the right may be made for wet conditions. Water pressure is dealt with by effective stress analysis.</p> <p>STRUCTURE</p>	<p>SURFACE CONDITIONS</p> <p>VERY GOOD Very rough, fresh unweathered surfaces</p> <p>GOOD Rough, slightly weathered, iron stained surfaces</p> <p>FAIR Smooth, moderately weathered and altered surfaces</p> <p>POOR Slickensided, highly weathered surfaces with compact coatings or fillings or angular fragments</p> <p>VERY POOR Slickensided, highly weathered surfaces with soft clay coatings or fillings</p> <p align="center">DECREASING SURFACE QUALITY →</p>					<p>GSI FOR HETEROGENEOUS ROCK MASSES SUCH AS FLYSCH (Marinos, P and Hoek E., 2000)</p> <p>From a description of the lithology, structure and surface conditions (particularly of the bedding planes), choose a box in the chart. Locate the position in the box that corresponds to the condition of the discontinuities and estimate the average value of GSI from the contours. Do not attempt to be too precise. Quoting a range from 33 to 37 is more realistic than giving GSI = 35. Note that the Hoek-Brown criterion does not apply to structurally controlled failures. Where unfavourably oriented continuous weak planar discontinuities are present, these will dominate the behaviour of the rock mass. The strength of some rock masses is reduced by the presence of groundwater and this can be allowed for by a slight shift to the right in the columns for fair, poor and very poor conditions. Water pressure does not change the value of GSI and it is dealt with by using effective stress analysis.</p> <p>COMPOSITION AND STRUCTURE</p>	<p>SURFACE CONDITIONS OF DISCONTINUITIES (Predominantly bedding planes)</p> <p>VERY GOOD - Very Rough, fresh unweathered surfaces</p> <p>GOOD - Rough, slightly weathered surfaces</p> <p>FAIR - Smooth, moderately weathered and altered surfaces</p> <p>POOR - Very smooth, occasionally slickensided surfaces with compact coatings or fillings with angular fragments</p> <p>VERY POOR - Very smooth, slickensided or highly weathered surfaces with soft clay coatings or fillings</p>				
<p>INTERLOCKING OF ROCK PIECES</p> <p align="center">↓ DECREASING INTERLOCKING OF ROCK PIECES</p> <div style="display: flex; flex-direction: column;"> <div style="margin-bottom: 5px;">  <p>INTACT OR MASSIVE - intact rock specimens or massive in situ rock with few widely spaced discontinuities</p> </div> <div style="margin-bottom: 5px;">  <p>BLOCKY - well interlocked undisturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets</p> </div> <div style="margin-bottom: 5px;">  <p>VERY BLOCKY - interlocked, partially disturbed mass with multi-faceted angular blocks formed by 4 or more joint sets</p> </div> <div style="margin-bottom: 5px;">  <p>BLOCKY/DISTURBED/SEAMY - folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity</p> </div> <div style="margin-bottom: 5px;">  <p>DISINTEGRATED - poorly interlocked, heavily broken rock mass with mixture of angular and rounded rock pieces</p> </div> <div style="margin-bottom: 5px;">  <p>LAMINATED/SHEARED - Lack of blockiness due to close spacing of weak schistosity or shear planes</p> </div> </div>	<p align="center">90</p> <p align="center">80</p> <p align="center">70</p> <p align="center">60</p> <p align="center">50</p> <p align="center">40</p> <p align="center">30</p> <p align="center">20</p> <p align="center">10</p>	<p align="center">N/A</p> <p align="center">N/A</p>	<p align="center">N/A</p> <p align="center">N/A</p>	<p align="center">N/A</p> <p align="center">N/A</p>	<p align="center">N/A</p> <p align="center">N/A</p>	<p>A. Thick bedded, very blocky sandstone The effect of pelitic coatings on the bedding planes is minimized by the confinement of the rock mass. In shallow tunnels or slopes these bedding planes may cause structurally controlled instability.</p> <p>B. Sandstone with thin inter-layers of siltstone</p> <p>C. Sandstone and siltstone in similar amounts</p> <p>D. Siltstone or silty shale with sandstone layers</p> <p>E. Weak siltstone or clayey shale with sandstone layers</p> <p>F. Tectonically deformed, intensively folded/faulted, sheared clayey shale or siltstone with broken and deformed sandstone layers forming an almost chaotic structure</p> <p>G. Undisturbed silty or clayey shale with or without a few very thin sandstone layers</p> <p>H. Tectonically deformed silty or clayey shale forming a chaotic structure with pockets of clay. Thin layers of sandstone are transformed into small rock pieces.</p> <p>→ Means deformation after tectonic disturbance</p>	<p align="center">70</p> <p align="center">60</p> <p align="center">50</p> <p align="center">40</p> <p align="center">30</p> <p align="center">20</p> <p align="center">10</p>	<p align="center">A</p> <p align="center">B</p> <p align="center">C</p> <p align="center">D</p> <p align="center">E</p> <p align="center">F</p> <p align="center">G</p> <p align="center">H</p>	<p align="center">A</p> <p align="center">B</p> <p align="center">C</p> <p align="center">D</p> <p align="center">E</p> <p align="center">F</p> <p align="center">G</p> <p align="center">H</p>	<p align="center">A</p> <p align="center">B</p> <p align="center">C</p> <p align="center">D</p> <p align="center">E</p> <p align="center">F</p> <p align="center">G</p> <p align="center">H</p>	



END PROJECT 17BP.5.R.69
-L- PT Sta. 18+50.00

NOTES:

- PLANS ADOPTED FROM ELECTRONIC FILES RECEIVED FROM MOTT MACDONALD DATED DECEMBER 2016.
- BRIDGE SKEW: 90°

FALCON ENGINEERING

FALCON ENGINEERING, INC.
1210 TRINITY ROAD, SUITE 110
RALEIGH, NC 27607

PHONE: 919.871.0800
FAX: 919.871.0803

BORING LOCATION PLAN

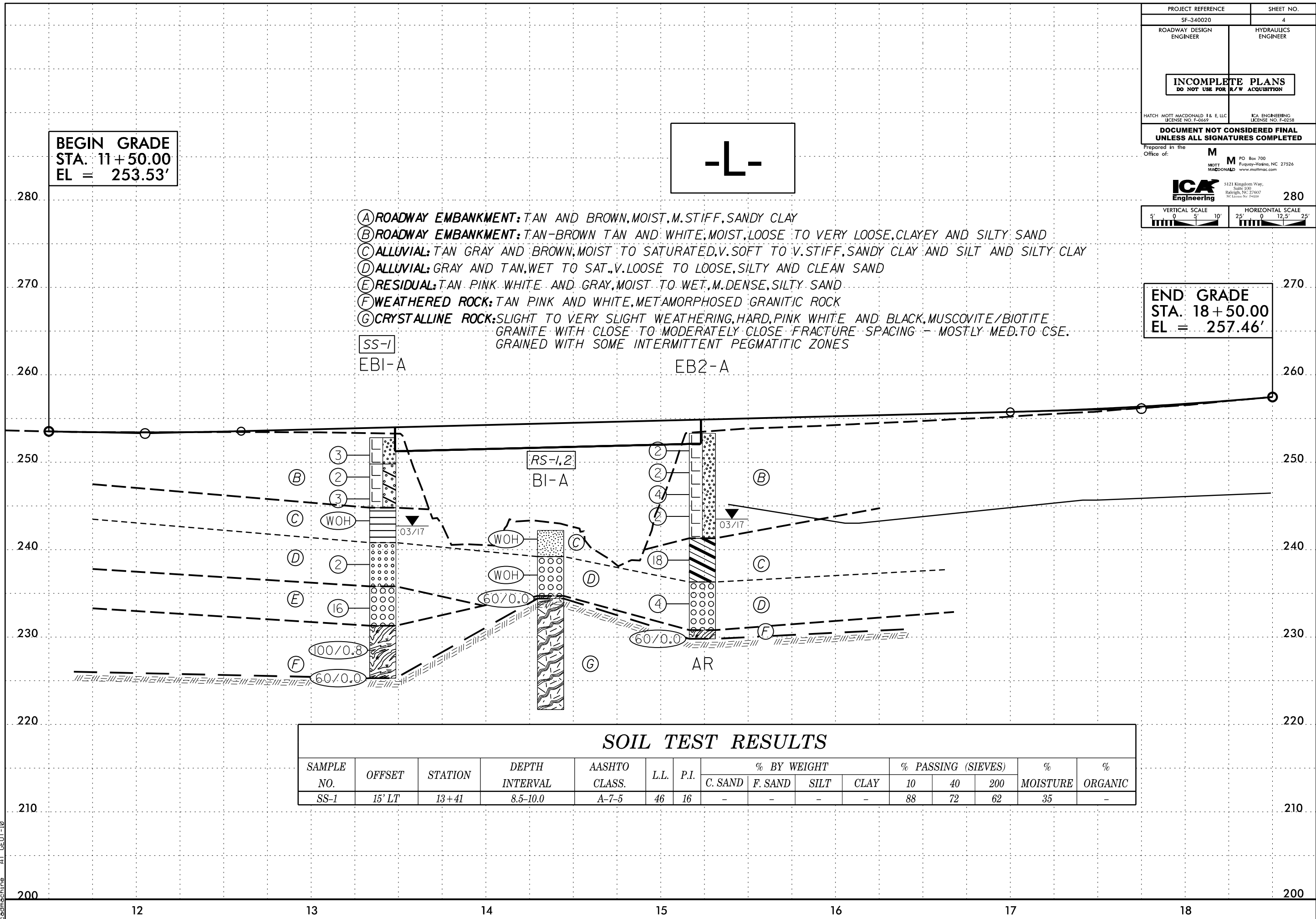
BRIDGE NO. 20 ON SR 1114 (PEACH ORCHARD RD.)
OVER CEDAR CREEK
FRANKLIN COUNTY, NORTH CAROLINA
WBS NO.: 17BP.5.R.69 | TIP NO.: SF-340020
FALCON PROJECT NO. G16029.03

BEGIN GRADE
STA. 11+50.00
EL = 253.53'

-L-

END GRADE
STA. 18+50.00
EL = 257.46'

- (A) ROADWAY EMBANKMENT: TAN AND BROWN, MOIST, M. STIFF, SANDY CLAY
- (B) ROADWAY EMBANKMENT: TAN-BROWN TAN AND WHITE, MOIST, LOOSE TO VERY LOOSE, CLAYEY AND SILTY SAND
- (C) ALLUVIAL: TAN GRAY AND BROWN, MOIST TO SATURATED, V. SOFT TO V. STIFF, SANDY CLAY AND SILT AND SILTY CLAY
- (D) ALLUVIAL: GRAY AND TAN, WET TO SAT., V. LOOSE TO LOOSE, SILTY AND CLEAN SAND
- (E) RESIDUAL: TAN PINK WHITE AND GRAY, MOIST TO WET, M. DENSE, SILTY SAND
- (F) WEATHERED ROCK: TAN PINK AND WHITE, METAMORPHOSED GRANITIC ROCK
- (G) CRYSTALLINE ROCK: SLIGHT TO VERY SLIGHT WEATHERING, HARD, PINK WHITE AND BLACK, MUSCOVITE/BIOTITE GRANITE WITH CLOSE TO MODERATELY CLOSE FRACTURE SPACING - MOSTLY MED. TO CSE. GRAINED WITH SOME INTERMITTENT PEGMATITIC ZONES



SOIL TEST RESULTS															
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	LL.	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1	15' LT	13+41	8.5-10.0	A-7-5	46	16	-	-	-	-	88	72	62	35	-

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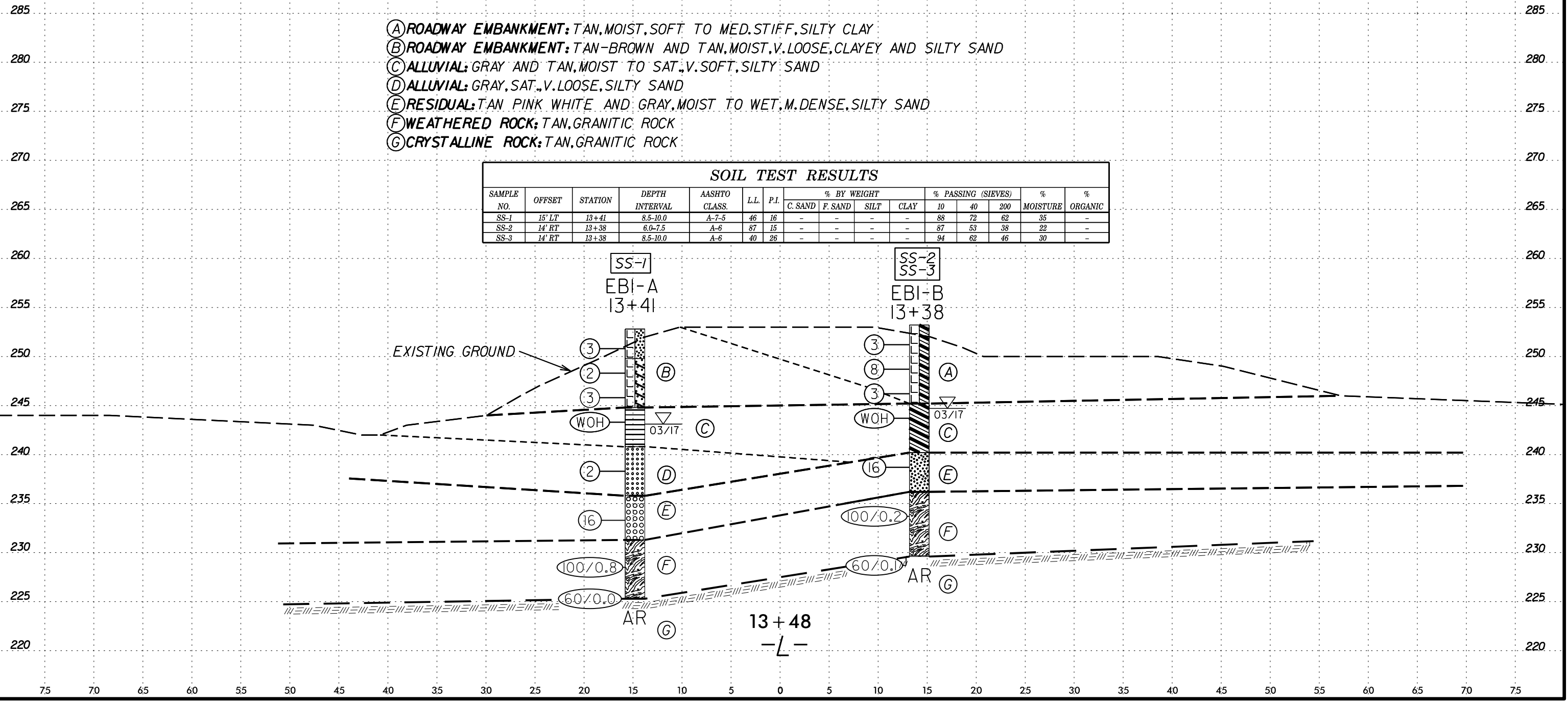
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EB1

- NOTES:**
- GROUNDLINE CROSS SECTION ALONG BENT LINE DRAWN FROM TOPOGRAPHIC DATA FROM ELECTRONIC FILES RECEIVED FROM MOTT MACDONALD DATED DECEMBER 2016.
 - INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS WITH BOTH PROJECTED ONTO THE CROSS SECTION.
 - BRIDGE SKEW: 90 DEGREES

- Ⓐ ROADWAY EMBANKMENT: TAN, MOIST, SOFT TO MED. STIFF, SILTY CLAY
- Ⓑ ROADWAY EMBANKMENT: TAN-BROWN AND TAN, MOIST, V. LOOSE, CLAYEY AND SILTY SAND
- Ⓒ ALLUVIAL: GRAY AND TAN, MOIST TO SAT., V. SOFT, SILTY SAND
- Ⓓ ALLUVIAL: GRAY, SAT., V. LOOSE, SILTY SAND
- Ⓔ RESIDUAL: TAN PINK WHITE AND GRAY, MOIST TO WET, M. DENSE, SILTY SAND
- Ⓕ WEATHERED ROCK: TAN, GRANITIC ROCK
- Ⓖ CRYSTALLINE ROCK: TAN, GRANITIC ROCK

SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING (SIEVES)			% MOISTURE	% ORGANIC
							C. SAND	F. SAND	SILT	CLAY	10	40	200		
SS-1	15' LT	13+41	8.5-10.0	A-7-5	46	16	-	-	-	-	88	72	62	35	-
SS-2	14' RT	13+38	6.0-7.5	A-6	87	15	-	-	-	-	87	53	38	22	-
SS-3	14' RT	13+38	8.5-10.0	A-6	40	26	-	-	-	-	94	62	46	30	-

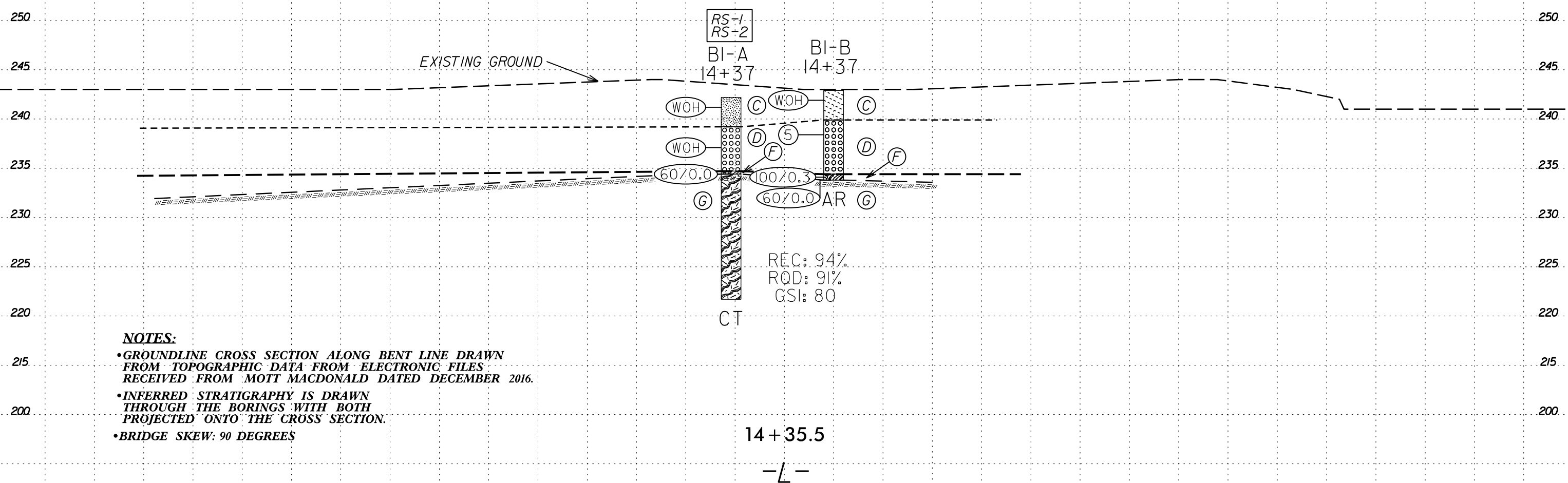


13+48
-L-

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codemachine

B1

- Ⓒ ALLUVIAL: BROWN, WET, V. SOFT, SANDY SILT
- Ⓓ ALLUVIAL: TAN, SAT., V. LOOSE TO LOOSE, CLEAN SAND
- Ⓕ WEATHERED ROCK: TAN, GRANITIC ROCK
- Ⓖ CRYSTALLINE ROCK: SLIGHT TO VERY SLIGHT WEATHERING, HARD, PINK WHITE AND BLACK, MUSCOVITE/BIOTITE, GRANITE WITH CLOSE TO MODERATELY CLOSE FRACTURE SPACING - MOSTLY MED. TO COARSE GRAINED WITH SOME INTERMITTENT PEGMATITIC ZONES



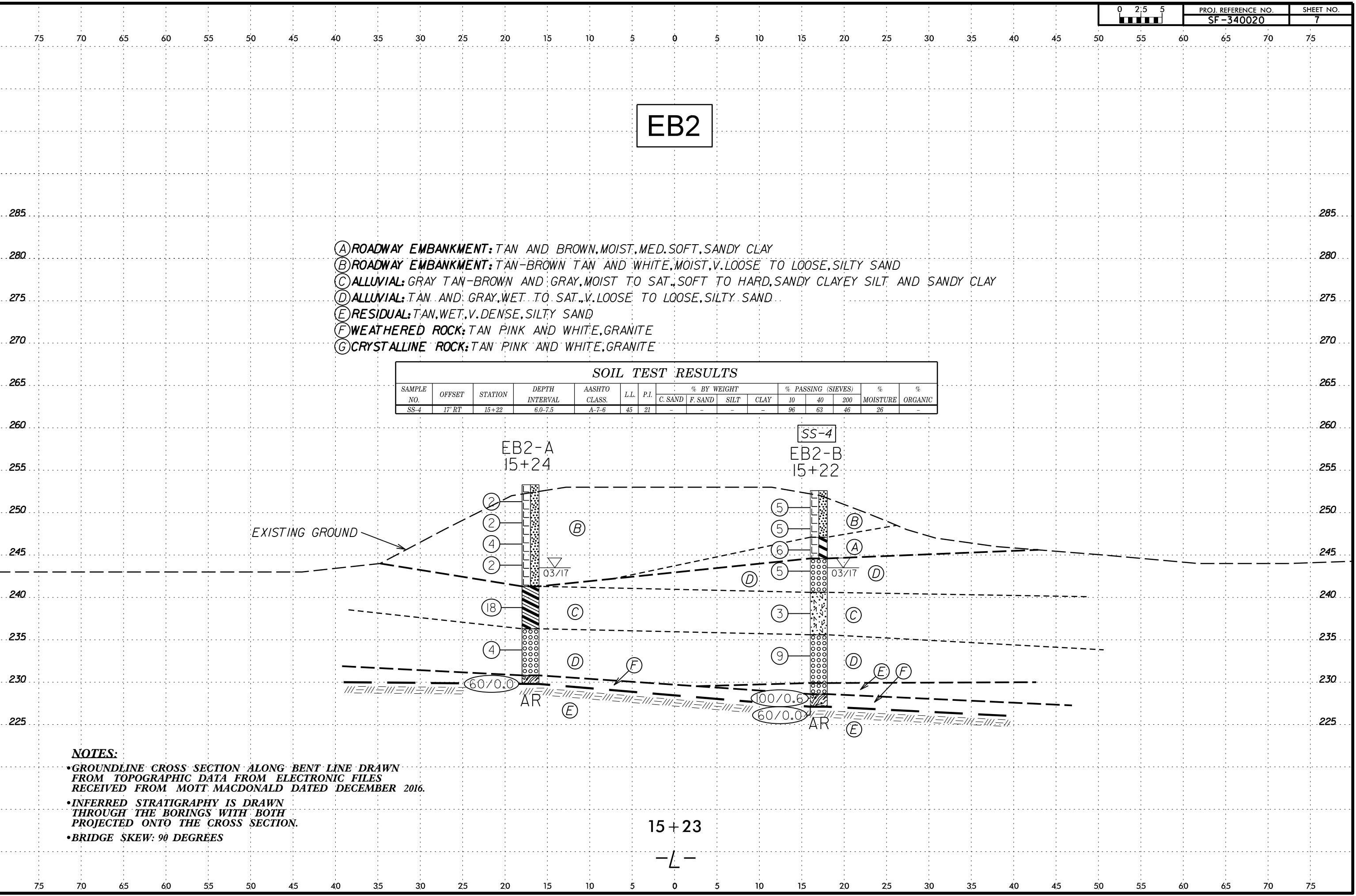
NOTES:

- GROUNDLINE CROSS SECTION ALONG BENT LINE DRAWN FROM TOPOGRAPHIC DATA FROM ELECTRONIC FILES RECEIVED FROM MOTT MACDONALD DATED DECEMBER 2016.
- INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS WITH BOTH PROJECTED ONTO THE CROSS SECTION.
- BRIDGE SKEW: 90 DEGREES

EB2

- (A) ROADWAY EMBANKMENT: TAN AND BROWN, MOIST, MED. SOFT, SANDY CLAY
- (B) ROADWAY EMBANKMENT: TAN-BROWN TAN AND WHITE, MOIST, V. LOOSE TO LOOSE, SILTY SAND
- (C) ALLUVIAL: GRAY TAN-BROWN AND GRAY, MOIST TO SAT., SOFT TO HARD, SANDY CLAYEY SILT AND SANDY CLAY
- (D) ALLUVIAL: TAN AND GRAY, WET TO SAT., V. LOOSE TO LOOSE, SILTY SAND
- (E) RESIDUAL: TAN, WET, V. DENSE, SILTY SAND
- (F) WEATHERED ROCK: TAN PINK AND WHITE, GRANITE
- (G) CRYSTALLINE ROCK: TAN PINK AND WHITE, GRANITE

SOIL TEST RESULTS															
SAMPLE NO.	OFFSET	STATION	DEPTH INTERVAL	AASHTO CLASS.	L.L.	P.I.	% BY WEIGHT				% PASSING (SIEVES)			%	%
							C. SAND	F. SAND	SILT	CLAY	10	40	200	MOISTURE	ORGANIC
SS-4	17' RT	15+22	6.0-7.5	A-7-6	45	21	-	-	-	-	96	63	46	26	-



NOTES:

- GROUNDLINE CROSS SECTION ALONG BENT LINE DRAWN FROM TOPOGRAPHIC DATA FROM ELECTRONIC FILES RECEIVED FROM MOTT MACDONALD DATED DECEMBER 2016.
- INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS WITH BOTH PROJECTED ONTO THE CROSS SECTION.
- BRIDGE SKEW: 90 DEGREES

15+23
 -L-

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GEOTECHNICAL BORING REPORT

BORE LOG

WBS 17BP.5.R.69		TIP SF-340020		COUNTY ALAMANCE		GEOLOGIST Goodnight, D.										
SITE DESCRIPTION BRIDGE NO. 20 ON SR 1114 (PEACH ORCHARD RD.) OVER CEDAR CREEK							GROUND WTR (ft)									
BORING NO. EB1-A		STATION 13+41		OFFSET 15 ft LT		ALIGNMENT -L-										
COLLAR ELEV. 252.8 ft		TOTAL DEPTH 27.5 ft		NORTHING 845,041		EASTING 2,182,725										
DRILL RIG/HAMMER EFF./DATE TRI8016 MOBILE B-57 97% 02/24/2017		DRILL METHOD H.S. Augers		HAMMER TYPE Automatic												
DRILLER Estep, J. E.		START DATE 03/29/17		COMP. DATE 03/29/17		SURFACE WATER DEPTH N/A										
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION	DEPTH (ft)	
			0.5ft	0.5ft	0.5ft	0	25	50	75	100						
255																
250	251.8	1.0	3	2	1								M	ROADWAY EMBANKMENT TAN-BROWN, SILTY CSE. TO F. SAND (A-2-4)	0.0	
	249.3	3.5	1	1	1								M	ROADWAY EMBANKMENT TAN, CLAYEY SAND (A-2-6) WITH TRACE GRAVEL	3.0	
245	246.8	6.0	1	1	2								M			
	244.3	8.5	1	1	WOH								SS-1	ALLUVIAL GRAY, SILTY CLAY (A-7-5) WITH LITTLE ORGANICS (WOOD FRAGS.)	8.0	
240	239.3	13.5	1	1	1								Sat.	GRAY, SLIGHTLY SILTY F. SAND (A-3) WITH TRACE ORGANICS	12.0	
235	234.3	18.5	7	8	8								W	RESIDUAL TAN AND PINK, SLIGHTLY SILTY F. TO CSE. SAND (A-1-b)	17.0	
230	229.3	23.5	42	58/0.3										WEATHERED ROCK TAN, GRANITE	21.5	
	225.3	27.5												Boring Terminated WITH STANDARD PENETRATION TEST REFUSAL at Elevation 225.3 ft ON CR: GRANITE	27.5	

WBS 17BP.5.R.69		TIP SF-340020		COUNTY ALAMANCE		GEOLOGIST Goodnight, D.										
SITE DESCRIPTION BRIDGE NO. 20 ON SR 1114 (PEACH ORCHARD RD.) OVER CEDAR CREEK							GROUND WTR (ft)									
BORING NO. EB1-B		STATION 13+38		OFFSET 14 ft RT		ALIGNMENT -L-										
COLLAR ELEV. 253.2 ft		TOTAL DEPTH 23.6 ft		NORTHING 845,023		EASTING 2,182,748										
DRILL RIG/HAMMER EFF./DATE TRI8016 MOBILE B-57 97% 02/24/2017		DRILL METHOD H.S. Augers		HAMMER TYPE Automatic												
DRILLER Estep, J. E.		START DATE 03/29/17		COMP. DATE 03/29/17		SURFACE WATER DEPTH N/A										
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION	DEPTH (ft)	
			0.5ft	0.5ft	0.5ft	0	25	50	75	100						
255																
250	252.2	1.0	2	2	1								M	ROADWAY EMBANKMENT TAN, SILTY SAND (A-6) WITH TRACE GRAVEL	0.0	
	249.7	3.5	2	4	4								M			
245	247.2	6.0	2	1	2								SS-2			
	244.7	8.5	2	1	WOH								SS-3	ALLUVIAL TAN AND GRAY, SILTY SAND (A-6)	8.0	
240	239.7	13.5	4	6	10								M	RESIDUAL GRAY AND WHITE, SILTY SAND (A-2-4) SAPROLITIC	13.0	
235	234.7	18.5												WEATHERED ROCK TAN, GRANITE	17.0	
230	229.7	23.5												CRYSTALLINE ROCK TAN, GRANITE	23.5	
														Boring Terminated WITH STANDARD PENETRATION TEST REFUSAL at Elevation 229.6 ft IN CR: GRANITE	23.6	

GEOTECHNICAL BORING REPORT BORE LOG

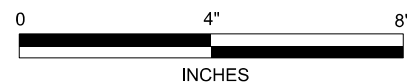
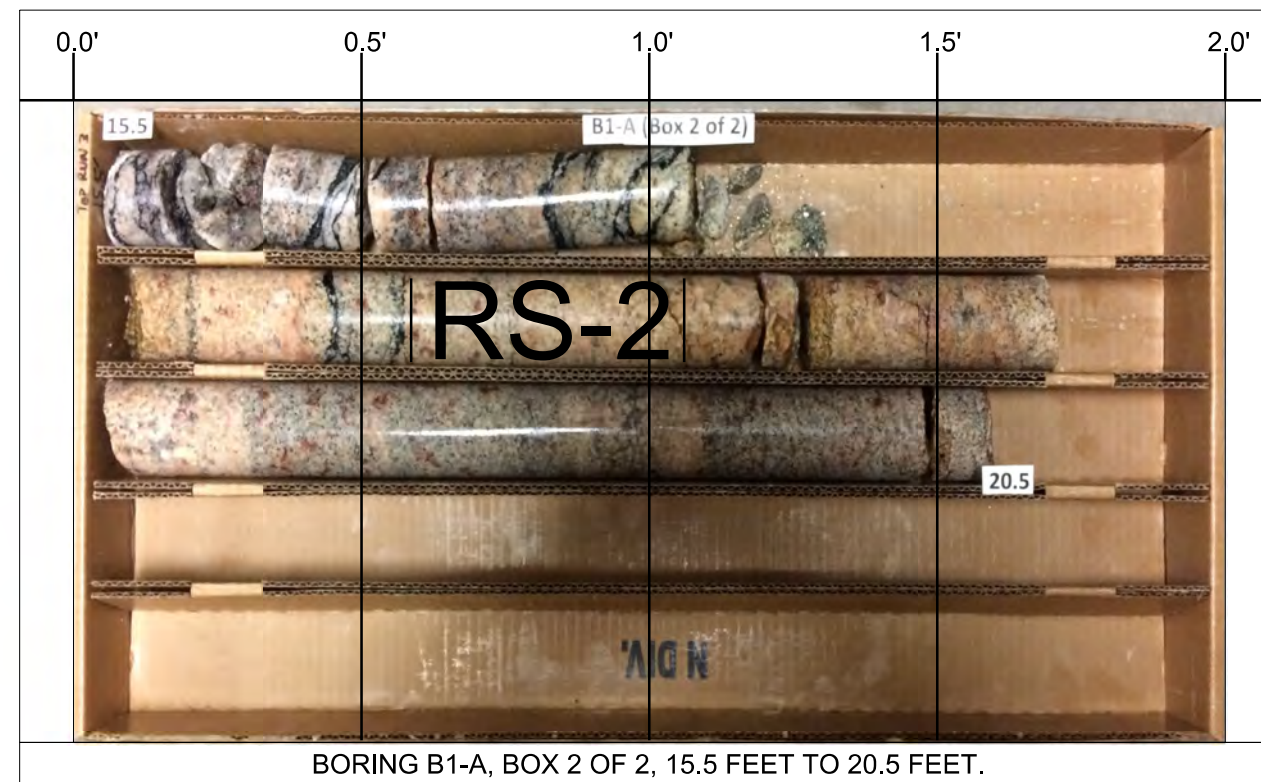
GEOTECHNICAL BORING REPORT CORE LOG

WBS 17BP.5.R.69		TIP SF-340020		COUNTY ALAMANCE		GEOLOGIST Goodnight, D.	
SITE DESCRIPTION BRIDGE NO. 20 ON SR 1114 (PEACH ORCHARD RD.) OVER CEDAR CREEK						GROUND WTR (ft)	
BORING NO. B1-A		STATION 14+37		OFFSET 5 ft LT		ALIGNMENT -L-	
COLLAR ELEV. 242.2 ft		TOTAL DEPTH 20.5 ft		NORTHING 845,115		EASTING 2,182,786	
DRILL RIG/HAMMER EFF./DATE TRI8016 MOBILE B-57 97% 02/24/2017		DRILL METHOD H.S. Augers		HAMMER TYPE Automatic			
DRILLER Estep, J. E.		START DATE 03/30/17		COMP. DATE 03/30/17		SURFACE WATER DEPTH N/A	

WBS 17BP.5.R.69		TIP SF-340020		COUNTY ALAMANCE		GEOLOGIST Goodnight, D.	
SITE DESCRIPTION BRIDGE NO. 20 ON SR 1114 (PEACH ORCHARD RD.) OVER CEDAR CREEK						GROUND WTR (ft)	
BORING NO. B1-A		STATION 14+37		OFFSET 5 ft LT		ALIGNMENT -L-	
COLLAR ELEV. 242.2 ft		TOTAL DEPTH 20.5 ft		NORTHING 845,115		EASTING 2,182,786	
DRILL RIG/HAMMER EFF./DATE TRI8016 MOBILE B-57 97% 02/24/2017		DRILL METHOD H.S. Augers		HAMMER TYPE Automatic			
DRILLER Estep, J. E.		START DATE 03/30/17		COMP. DATE 03/30/17		SURFACE WATER DEPTH N/A	

ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION	DEPTH (ft)	
			0.5ft	0.5ft	0.5ft	0	25	50	75	100						
245																
240	242.2	0.0	WOH	WOH	WOH	0							W		242.2	0.0
235	238.1	4.1	WOH	WOH	WOH	0							Sat.		239.2	3.0
230	234.4	7.8	60/0.0										RS-1		234.4	7.8
225													RS-2		221.7	20.5

ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	RUN		SAMP. NO.	STRATA		LOG	DESCRIPTION AND REMARKS	DEPTH (ft)
					REC. (%)	RQD (%)		REC. (%)	RQD (%)			
234.4											Begin Coring @ 7.8 ft	
	234.4	7.8	2.7	3:01/0.7	(2.5)	(2.4)		(12.0)	(11.5)		CRYSTALLINE ROCK	7.8
	231.7	10.5	5.0	4:34/1.0	93%	89%		94%	91%		SLIGHT TO VERY SLIGHT WEATHERING, HARD, PINK WHITE AND BLACK, MUSCOVITE/BIOTITE GRANITE WITH CLOSE TO MODERATELY CLOSE FRACTURE SPACING - MOSTLY MED. TO CSE. GRAINED WITH SOME INTERMITTENT PEGMATITIC ZONES	
230				5:57/1.0			RS-1				REC = 94%, RQD = 91%, GSI = 80	
	226.7	15.5	5.0	5:41/1.0	(5.0)	(5.0)						
	225			6:23/1.0	100%	100%						
	222.7	20.5	5.0	8:25/1.0			RS-2					
	221.7			9:37/1.0	(4.5)	(4.1)						
				8:59/1.0	90%	82%						
	221.7			15:30/1.0							Boring Terminated at Elevation 221.7 ft IN CR: GRANITE	20.5
				6:24/1.0								
				3:54/1.0								
				5:58/1.0								
				5:11/1.0								



FALCON
ENGINEERING

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1210 TRINITY ROAD, SUITE 110
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PHONE: 919.871.0800
FAX: 919.871.0803

ROCK CORE PHOTOGRAPHS

BRIDGE NO. 20 ON SR 1114 (PEACH ORCHARD RD.)
OVER CEDAR CREEK
FRANKLIN COUNTY, NORTH CAROLINA
WBS NO.: 17BP.5.R.69 | TIP NO.: SF-340020
FALCON PROJECT NO. G16029.03

GEOTECHNICAL BORING REPORT

BORE LOG

WBS 17BP.5.R.69		TIP SF-340020		COUNTY ALAMANCE		GEOLOGIST Goodnight, D.									
SITE DESCRIPTION BRIDGE NO. 20 ON SR 1114 (PEACH ORCHARD RD.) OVER CEDAR CREEK						GROUND WTR (ft)									
BORING NO. B1-B		STATION 14+37		OFFSET 5 ft RT		ALIGNMENT -L-									
COLLAR ELEV. 242.9 ft		TOTAL DEPTH 9.1 ft		NORTHING 845,109		EASTING 2,182,794									
DRILL RIG/HAMMER EFF./DATE TRI8016 MOBILE B-57 97% 02/24/2017		DRILL METHOD H.S. Augers		HAMMER TYPE Automatic											
DRILLER Estep, J. E.		START DATE 03/30/17		COMP. DATE 03/30/17		SURFACE WATER DEPTH N/A									
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG MOI	LOG G	SOIL AND ROCK DESCRIPTION	
			0.5ft	0.5ft	0.5ft	0	25	50	75	100					
245															
240	242.9	0.0	WOH	WOH	WOH	0							W		242.9 0.0
	239.4	3.5	2	2	3	5							Sat.		239.9 3.0
235	234.4	8.5	100/0.3												234.4 8.5
	233.8	9.1	60/0.0												233.8 9.1
															WEATHERED ROCK TAN, GRANITE Boring Terminated WITH STANDARD PENETRATION TEST REFUSAL at Elevation 233.8 ft ON CR: GRANITE

WBS 17BP.5.R.69		TIP SF-340020		COUNTY ALAMANCE		GEOLOGIST Goodnight, D.									
SITE DESCRIPTION BRIDGE NO. 20 ON SR 1114 (PEACH ORCHARD RD.) OVER CEDAR CREEK						GROUND WTR (ft)									
BORING NO. EB2-A		STATION 15+24		OFFSET 17 ft LT		ALIGNMENT -L-									
COLLAR ELEV. 253.3 ft		TOTAL DEPTH 23.5 ft		NORTHING 845,194		EASTING 2,182,825									
DRILL RIG/HAMMER EFF./DATE TRI8016 MOBILE B-57 97% 02/24/2017		DRILL METHOD H.S. Augers		HAMMER TYPE Automatic											
DRILLER Estep, J. E.		START DATE 03/28/17		COMP. DATE 03/28/17		SURFACE WATER DEPTH N/A									
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG MOI	LOG G	SOIL AND ROCK DESCRIPTION	
			0.5ft	0.5ft	0.5ft	0	25	50	75	100					
255															
	253.3	0.0													253.3 0.0
250	252.3	1.0	1	1	1	2							M		ROADWAY EMBANKMENT TAN-BROWN SILTY SAND (A-2-4) WITH TRACE GRAVEL AND LITTLE MICA
	249.8	3.5	1	1	1	4							M		
	247.3	6.0	2	2	2								M		
245	244.8	8.5	1	1	1	2									244.8 8.5
240	239.8	13.5	6	9	9	18							M		239.8 13.5
235	234.8	18.5	2	2	2	4							Sat.		234.8 18.5
230	229.8	23.5	60/0.0												229.8 23.5
															WEATHERED ROCK PINK AND WHITE GRANITE Boring Terminated WITH STANDARD PENETRATION TEST REFUSAL at Elevation 229.8 ft ON CR: GRANITE

NCDOT BORE DOUBLE BR20 FRANKLIN.GPJ NC_DOT.GDT 8/25/17



LABORATORY TEST RESULTS
 Bridge No. 20 over Cedar Cr. on SR 1114
 Franklin County, North Carolina
 Falcon Engineering Project Number: G16029.03
 June 8, 2017

UNIAXIAL COMPRESSIVE STRENGTH OF INTACT ROCK CORE SPECIMENS *Performed in General Accordance with ASTM D7012*

Sample ID.: RÙ-1
 Location: B1-A
 Depth (ft): 10.5-11.0

Length (in.): 4.36
 Diameter (in.): 1.98
 Area (in²): 3.079
 L/D 2.20
 Unit Weight (pcf): 161.5

Compressive Strength (psi): 18910
 Time to Failure, mins:sec: 10:46

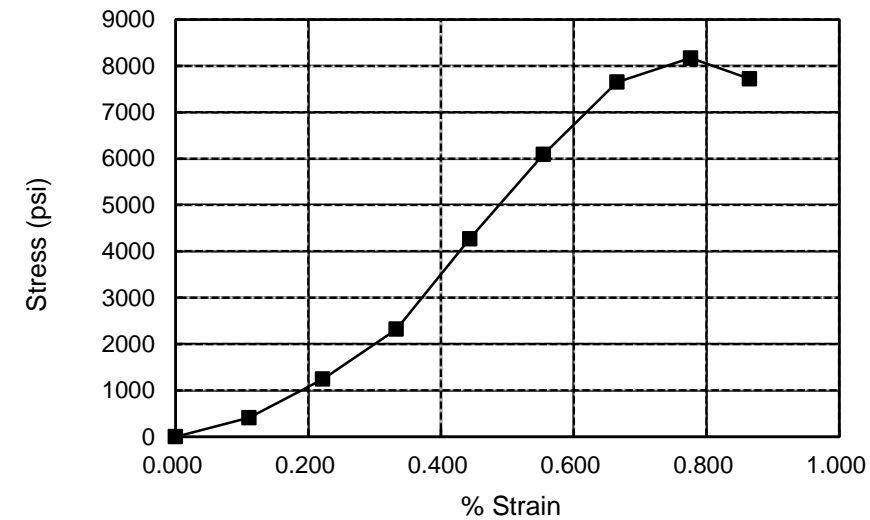
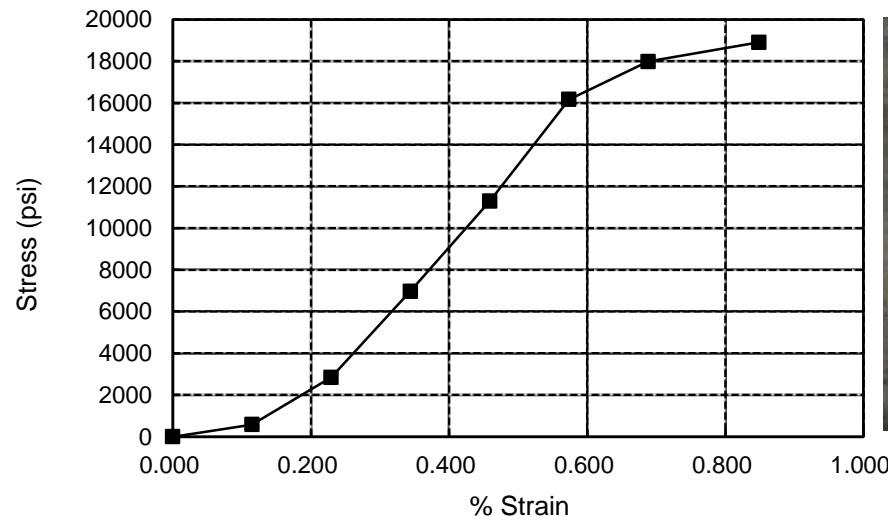
Deflection (in.)	Strain (%)	Load (lbf)	Compressive Strength (psi)	Young's Modulus (psi)
0.000	0.000	0	0	
0.005	0.115	1780	580	505,760
0.010	0.229	8740	2840	1,238,240
0.015	0.344	21470	6970	2,025,947
0.020	0.459	34750	11290	2,461,220
0.025	0.573	49780	16170	2,820,048
0.030	0.688	55400	17990	2,614,547
0.037	0.849	58220	18910	2,228,314

Sample ID.: RÙ-2
 Location: B1-A
 Depth (ft): 16.5-17.0

Length (in.): 4.51
 Diameter (in.): 1.98
 Area (in²): 3.079
 L/D 2.28
 Unit Weight (pcf): 162.9

Compressive Strength (psi): 8170
 Time to Failure, mins:sec: 8:25

Deflection (in.)	Strain (%)	Load (lbf)	Compressive Strength (psi)	Young's Modulus (psi)
0.000	0.000	0	0	
0.005	0.111	1260	410	369,820
0.010	0.222	3810	1240	559,240
0.015	0.333	7150	2320	697,547
0.020	0.443	13140	4270	962,885
0.025	0.554	18760	6090	1,098,636
0.030	0.665	23560	7650	1,150,050
0.035	0.776	25160	8170	1,052,763
0.039	0.865	23780	7720	892,749



Remarks:

*Young's modulus is calculated using the secant modulus at each data point per Figure 2 (C) in ASMTM D 7012

Reviewed by: *John Aailly*